



POLITECNICO
MILANO 1863

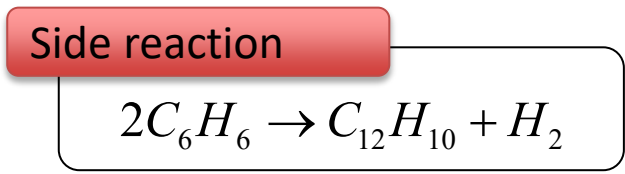
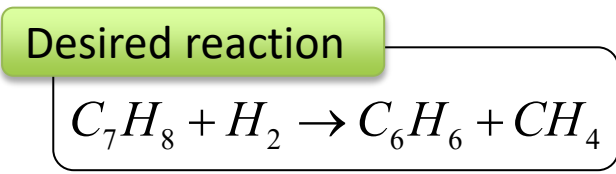
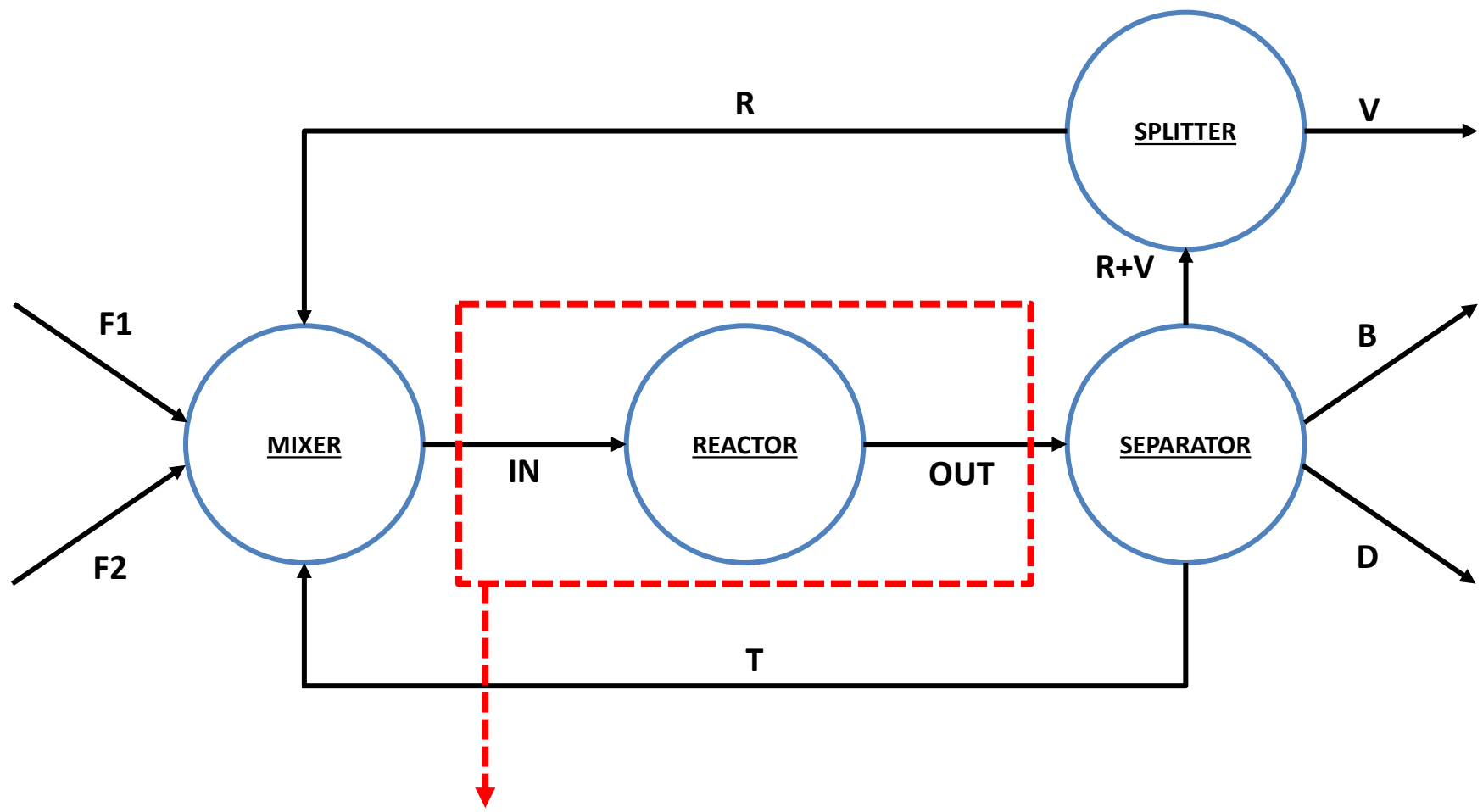
LAB2: Reactor design

Designing the hydrodealkylator

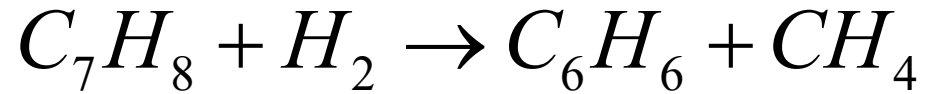
Process Systems Engineering A – Prof. Davide Manca

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Desired reaction



$$R_1 = k_1 C_{C_7H_8} \sqrt{C_{H_2}}$$

[kmol/(m³ · s)]

$$k_1 = A_1 \exp\left(-\frac{E_1}{RT}\right) [\text{m}^{1.5}/(\text{kmol}^{0.5} \cdot \text{s})]$$

$$A_1 = 3.5 \cdot 10^{10} [\text{m}^{1.5}/(\text{kmol}^{0.5} \cdot \text{s})]$$

$$E_1 = 50900 [\text{kcal}/\text{kmol}]$$

Side reaction



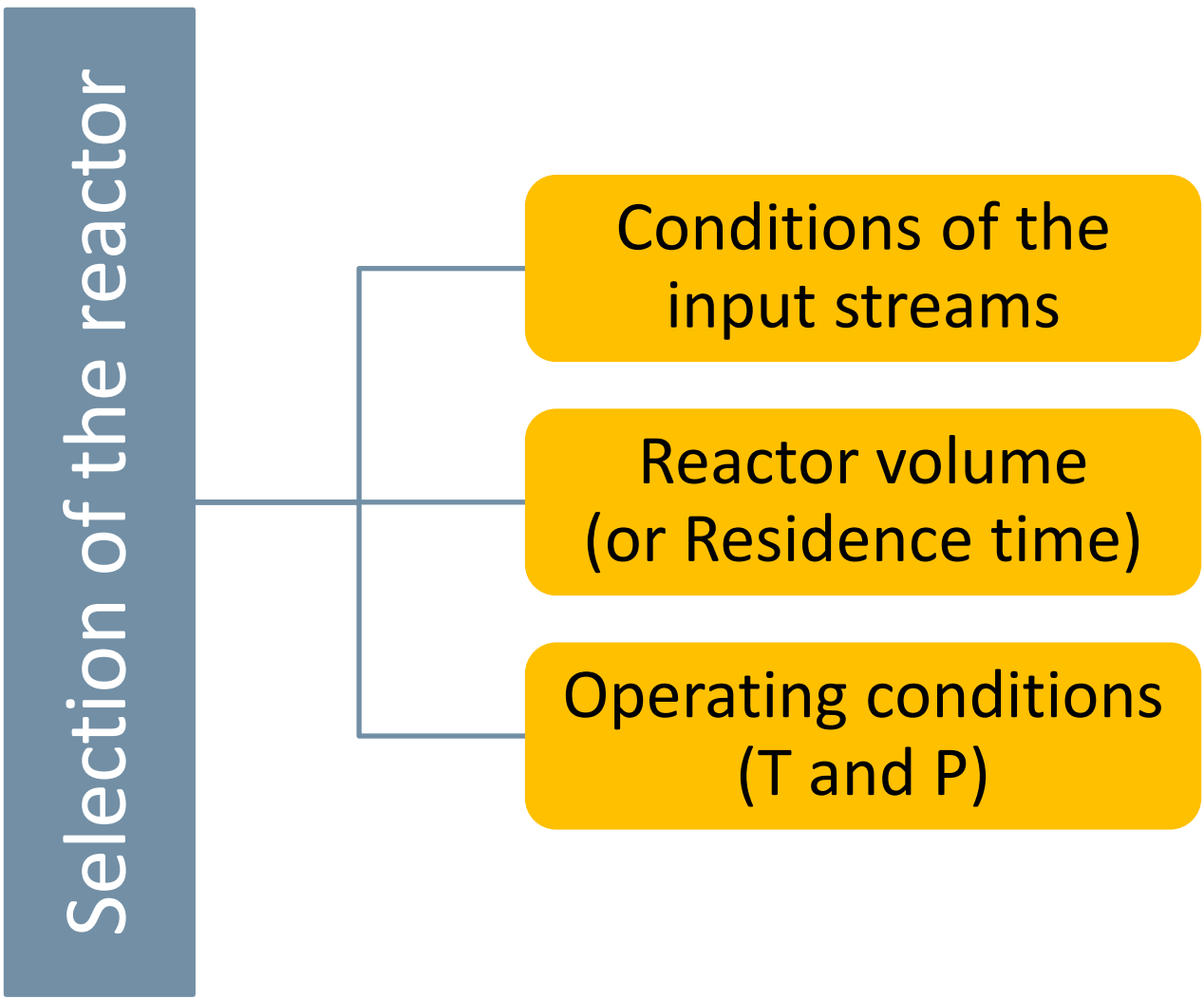
$$R_2 = k_2 C_{C_6H_6}^2$$

[kmol/(m³ · s)]

$$k_2 = A_2 \exp\left(-\frac{E_2}{RT}\right) [\text{m}^3/(\text{kmol} \cdot \text{s})]$$

$$A_2 = 2.1 \cdot 10^{12} [\text{m}^3/(\text{kmol} \cdot \text{s})]$$

$$E_2 = 60500 [\text{kcal}/\text{kmol}]$$



Conditions of the input streams

- The stream of fresh hydrogen (F1) contains 5%_{mol} of methane;
- The reactants are at ambient temperature;
- The Hydrogen-to-Toluene Ratio (HTR) at the inlet of the reactor must be equal to 5.

Reactor volume (and Residence time)

- Benzene selectivity must be $\geq 96\%$;
- Benzene productivity must be 265 kmol/h.

Operating conditions

Pressure

- Both reactions are equimolar.
- ⇒ $P = 34 \text{ bar}$

Temperature

- No need for any catalyst;
 - The desired reaction is exothermic;
 - The side reaction is faster at high T (higher E_a).
- ⇒ it is worth operating at **low temperatures!**



Range of interest: $600\text{--}750^\circ\text{C}$ ⇒ carry out tests with $\Delta T = 50^\circ\text{C}$

The reaction scheme is in series:
Toluene $\xrightarrow{\text{Reaction \#1}}$ Benzene $\xrightarrow{\text{Reaction \#2}}$ Biphenyl



The control of residence time is fundamental
($\sigma_{\text{C}_6\text{H}_6}$ must be kept $\geq 96\%$)



a Plug Flow Reactor (PFR) is needed

PFR: 5 species → 5 ODEs

$$\left\{ \begin{aligned} \frac{dF_{H_2}}{dV} &= \nu_{1,H_2} R_1(T, P, \mathbf{x}) + \nu_{2,H_2} R_2(T, P, \mathbf{x}) \\ \frac{dF_{CH_4}}{dV} &= \nu_{1,CH_4} R_1(T, P, \mathbf{x}) \\ \frac{dF_{C_7H_8}}{dV} &= \nu_{1,C_7H_8} R_1(T, P, \mathbf{x}) \\ \frac{dF_{C_6H_6}}{dV} &= \nu_{1,C_6H_6} R_1(T, P, \mathbf{x}) + \nu_{2,C_6H_6} R_2(T, P, \mathbf{x}) \\ \frac{dF_{C_{12}H_{10}}}{dV} &= \nu_{2,C_{12}H_{10}} R_2(T, P, \mathbf{x}) \end{aligned} \right.$$

$$\left\{ \begin{aligned} F_{H_2}(V=0) &= F_{H_2}^{IN} \\ F_{CH_4}(V=0) &= F_{CH_4}^{IN} \\ F_{C_7H_8}(V=0) &= F_{C_7H_8}^{IN} \\ F_{C_6H_6}(V=0) &= 0 \\ F_{C_{12}H_{10}}(V=0) &= 0 \end{aligned} \right.$$

$$\left\{ \begin{aligned} F_{H_2}(V=V_{tot}) &= F_{H_2}^{OUT} \\ F_{CH_4}(V=V_{tot}) &= F_{CH_4}^{OUT} \\ F_{C_7H_8}(V=V_{tot}) &= F_{C_7H_8}^{OUT} \\ F_{C_6H_6}(V=V_{tot}) &= F_{C_6H_6}^{OUT} \\ F_{C_{12}H_{10}}(V=V_{tot}) &= F_{C_{12}H_{10}}^{OUT} \end{aligned} \right.$$

Also, remember:

$$\sigma_{C_6H_6} = \frac{F_{C_6H_6}}{F_{C_7H_8}^{IN} - F_{C_7H_8}^{OUT}}$$

Selectivity

$$\chi_{C_7H_8} = \frac{F_{C_7H_8}^{IN} - F_{C_7H_8}^{OUT}}{F_{C_7H_8}^{IN}}$$

Conversion

$$\tau = \frac{V}{\dot{V}}$$

Residence time