



Associazione professionale Italiana Ambiente e Sicurezza
Comitato C 4.3 Energia e fonti rinnovabili

CONVEGNO AIAS

Milano, 18 Maggio 2012

cmr Gexcon



 **POLITECNICO DI MILANO**



The Viareggio railway accident Lessons-learnt

Davide Manca

- Fenomenologia dell'incidente
- Modellazione matematica
- Risultati della simulazione
- Analisi e modellazione delle incertezze
- Conclusioni

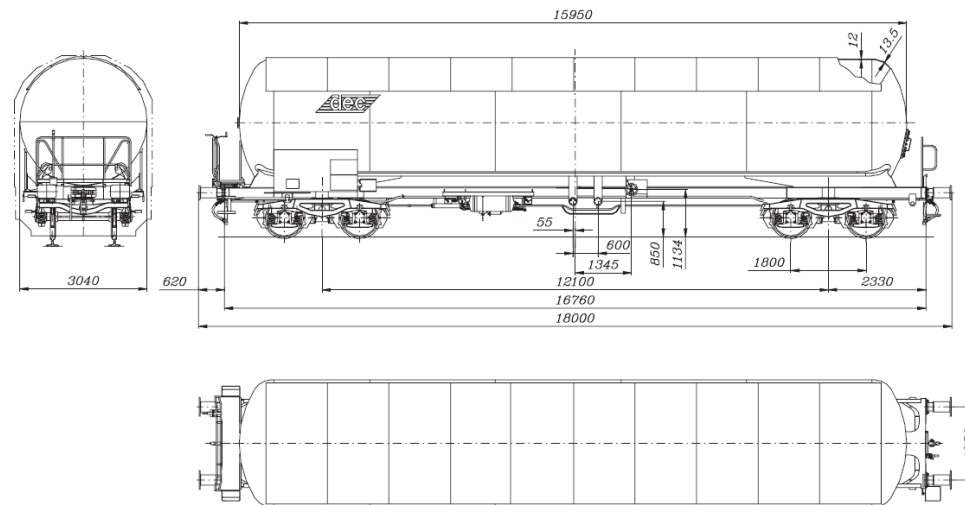




Fenomenologia dell'incidente



- 29 Giugno 2009 tardo pomeriggio un convoglio merci carico di GPL lascia la raffineria Sarpom di Trecate (NO) diretto a Gricignano (CE) verso il deposito della Aversana Petroli (contratto trasporto con FS Logistica per due trasporti settimanali per 48 settimane all'anno).
- Il convoglio è costituito da:
 - una locomotiva E655
 - 14 vagoni (ferrocisterne) di capacità nominale pari a 110 m³/cad
- Quantitativo totale di GPL trasportato 630 t





- Durante l'attraversamento della stazione di Viareggio verso mezzanotte l'asse frontale della prima ferrocisterna cede improvvisamente



- Sette ferrocisterne deragliate: 5 rovesciate e due sviaate
- Sette ferrocisterne ancora su binario
- Intercorrono 590 m tra il punto iniziale di cedimento e la testa del convoglio



- Il primo vagone deragliato e rovesciatosi striscia lungo la massicciata ed urta una trave (binario) a doppia T conficcata nel terreno (a fini misurazione e posa binari) che sporge dal terreno per circa 30 cm









locomotore

#1





















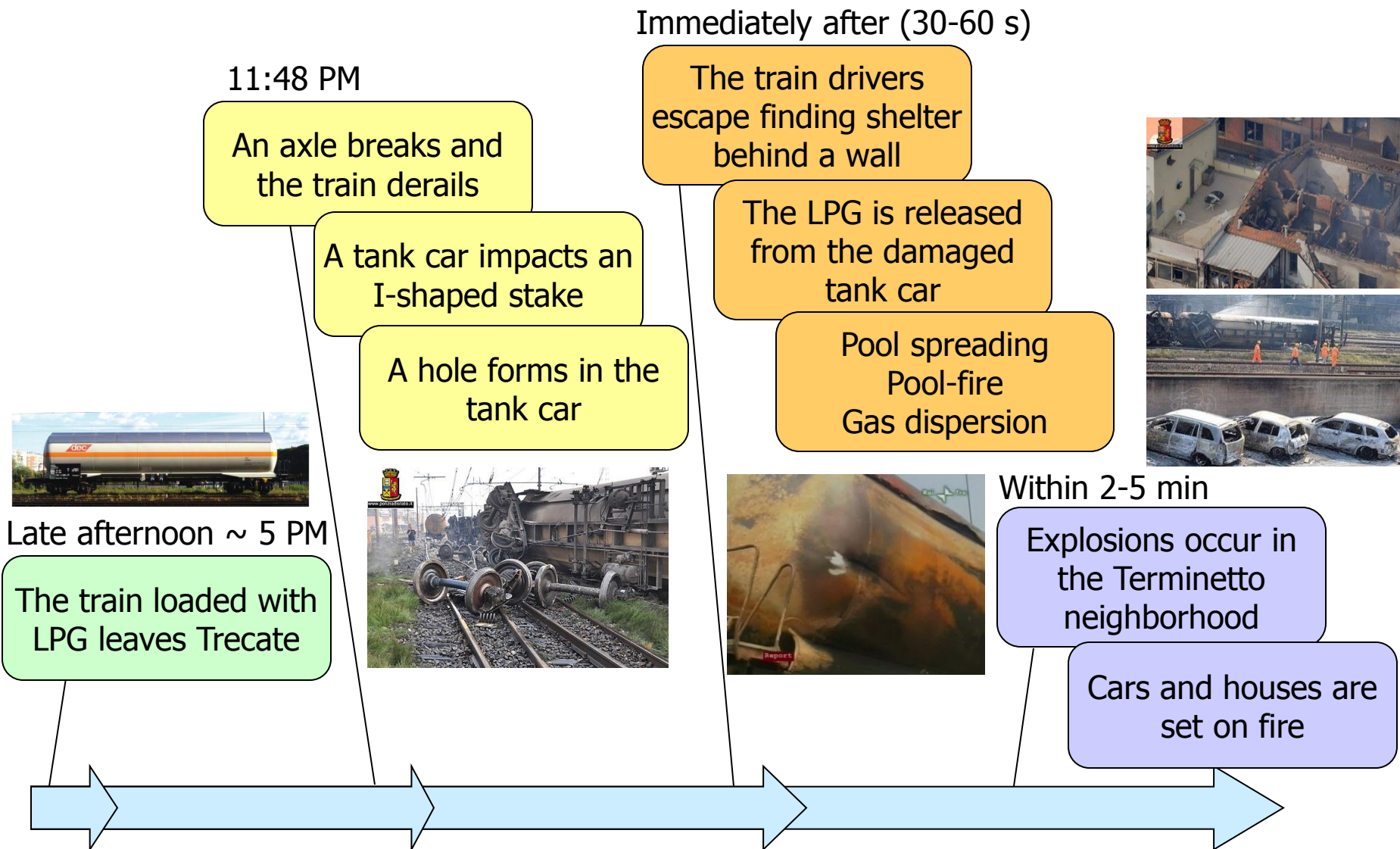




- **32 fatalities**
 - **14 people died immediately**
 - some were literally run over by flame radiation
 - collapse of the buildings
 - inhalation of toxic substances from the burning of houses
 - **2 heart attacks**
 - the **last person** died **six months after** the accident
- More than **thirty people** were **seriously injured**
- **1100 people** had to **evacuate** their homes for safety reasons
- Infrastructure **overall damage** was valued at **32 M€**.



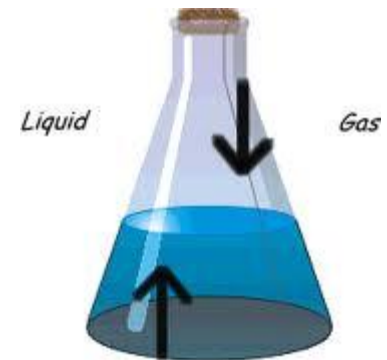
Modellazione matematica

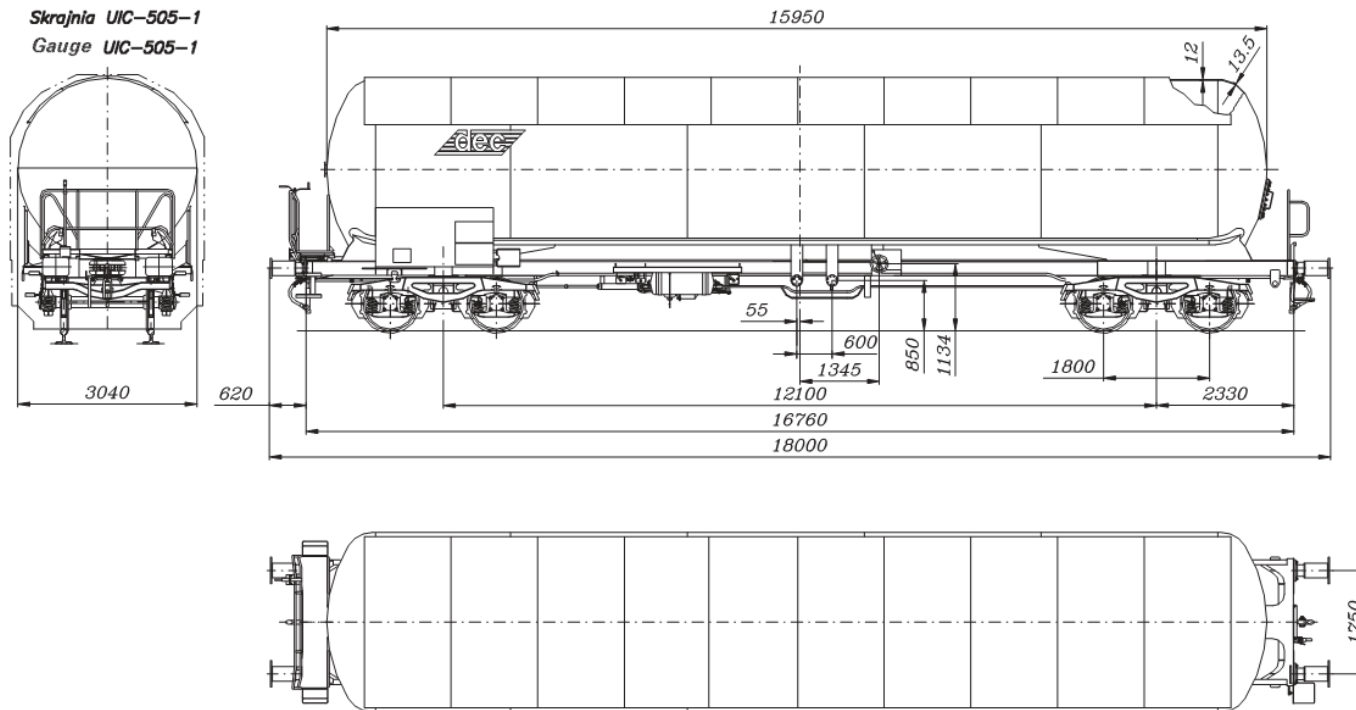




Models for the description of:

- Thermodynamics and V-L equilibrium
- Thermal dispersion
- The source term $\rightarrow$ outflow
- Jet flash $\rightarrow$ L + V fractions with rainout
- Spreading and shrinking of the liquid pool
- Flash fire and pool-fire
- Radiative heat transfer to the tank car
- Irregular terrain and ballast roughness
- Dense gas dispersion in complex environments
- Calm wind conditions







LPG composition

LPG is a variable mixture of C₃ and C₄ isomers



Pure n-propane

Storage conditions

Pressure [bar]	Temperature	
9	296.15 K	23.00 °C
15	317.10 K	43.95 °C
20	330.51 K	57.36 °C
25	341.69 K	68.54 °C

← Ambient conditions

← Working pressure

Total tank capacity	110 m ³
Calculation pressure	25 bar
Working pressure	25 bar
Test over-pressure	25 bar
External over-pressure	1 bar



23 °C, 9 bar

www.gatx.com



Mass in the punctured tank car

The train transported 630 tons of
LPG distributed in 14 tank cars



45 tons

Hole equivalent area

Only a portion of the longitudinal
mark was cut open



100 cm² trapezoidal hole
 $c_D = 0.62$ (jagged-in sheet)





Ignition time

Some witnesses declared that the ignition occurred 2 min after the derailment, someone else reported 5 min

The intense emotional agitation of the witnesses in those moments did not allow analyzing objectively the course of events



2 min





Wind speed and direction

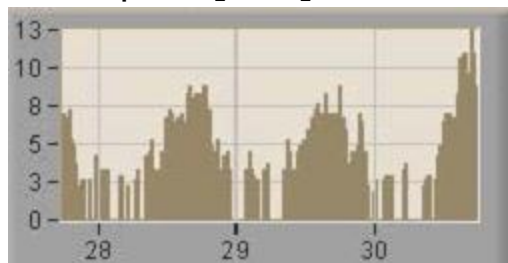
Report measured at the top of a hotel on the seafront, 1.7 km from the epicenter of the accident

Wind direction	NEE
Wind speed [m/s]	< 1
Air temperature [°C]	23
Ambient pressure [mbar]	1008
Relative humidity	80%

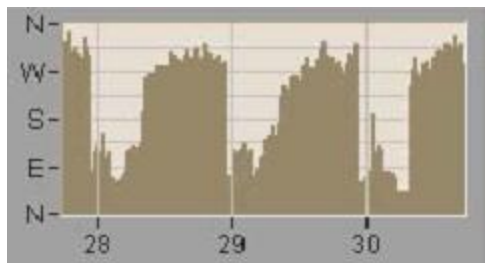


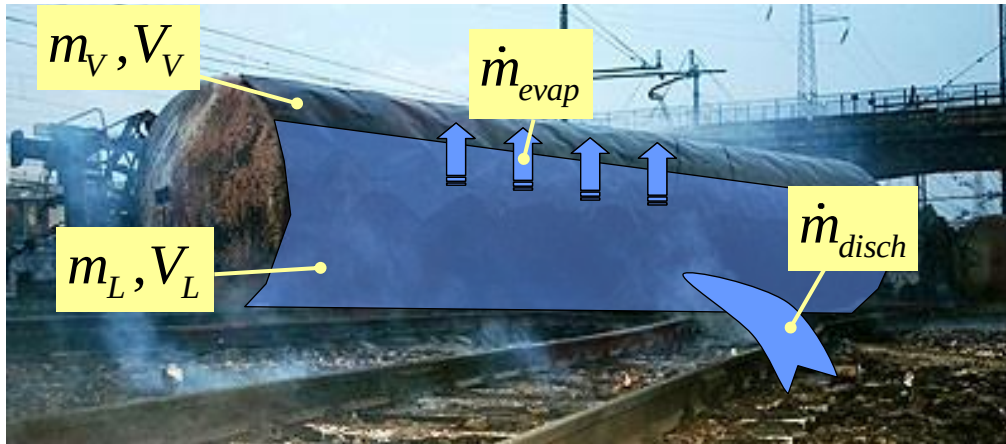
0.5 m/s, NEE

Wind speed [knot]



Wind direction





Mass balance
Energy balance
Volume conservation

$$\left\{ \begin{array}{l} \frac{dm_L}{dt} = - \frac{\dot{m}_{disch}}{\left(1 - \frac{\rho_V}{\rho_L}\right)} \end{array} \right.$$

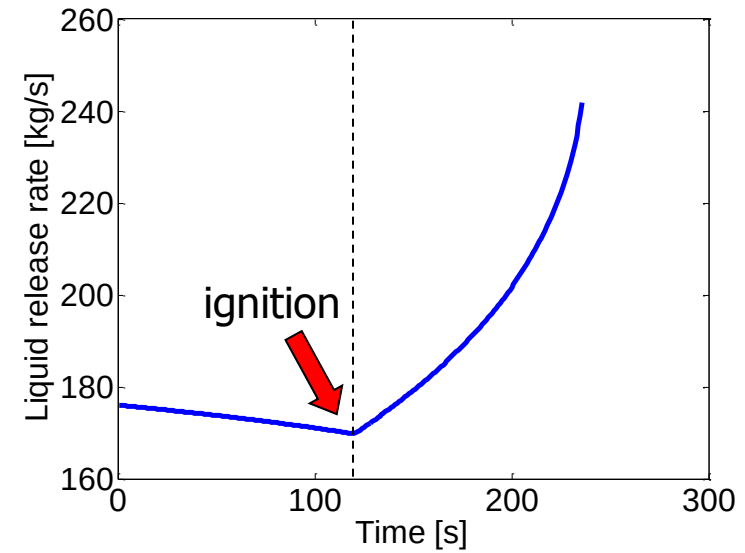
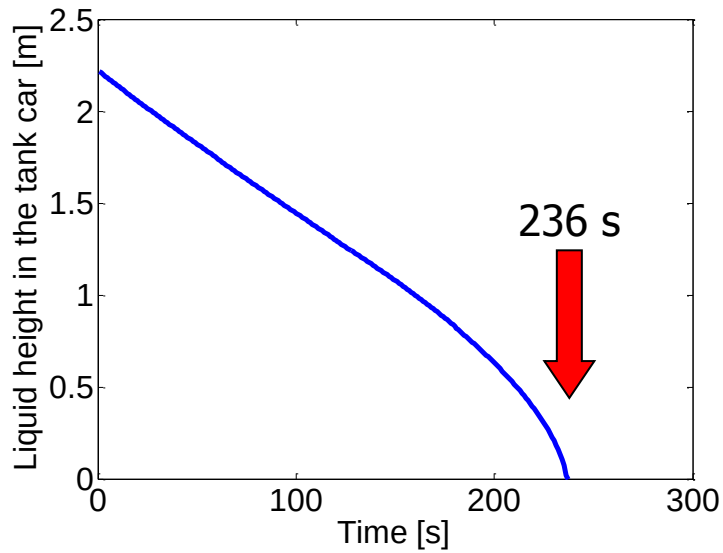
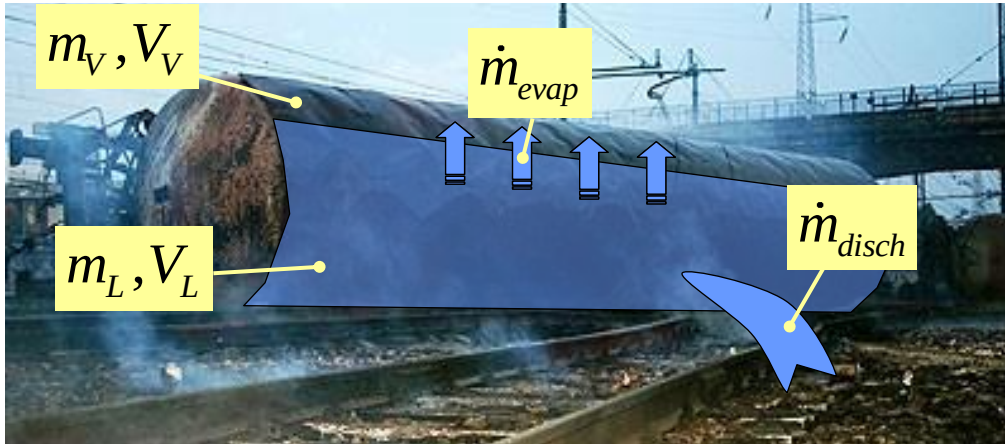
$$\frac{dm_V}{dt} = \dot{m}_{evap}$$

$$\frac{dT}{dt} = - \frac{\dot{m}_{evap} \Delta H_{ev} + \alpha Q_{irr} A}{m_L c p_L + m_V c p_V}$$

$$\dot{m}_{disch} = \rho_L A_h c_D \sqrt{\frac{2}{\rho_L} (P - P_a) + 2gh_L}$$

$$\dot{m}_{evap} = - \frac{dm_L}{dt} \frac{\rho_V}{\rho_L}$$

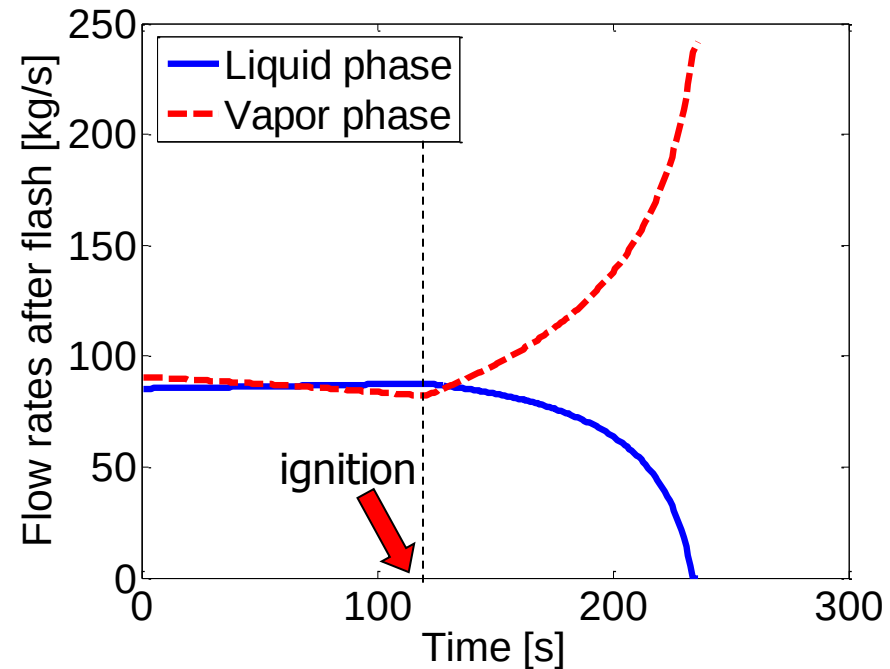
$$V_L = L \left[R^2 \arccos(1 - h_L/R) - (R - h_L) \sqrt{2Rh_L - h_L^2} \right]$$



Hypotheses

- Jet flash downstream the emission from the hole
- No liquid entrainment in the vapor phase

$$\begin{cases} x_V = \frac{cp_L (T - T_{eb})}{\Delta H_{ev}} \\ x_L = 1 - \frac{cp_L (T - T_{eb})}{\Delta H_{ev}} \end{cases}$$



Pool shape

The liquid fraction spread on an irregular terrain and found some obstacles that limited a symmetric spreading

The liquid was partially absorbed by the permeable ballast made of pebbles and rocks



Circular, unconfined pool

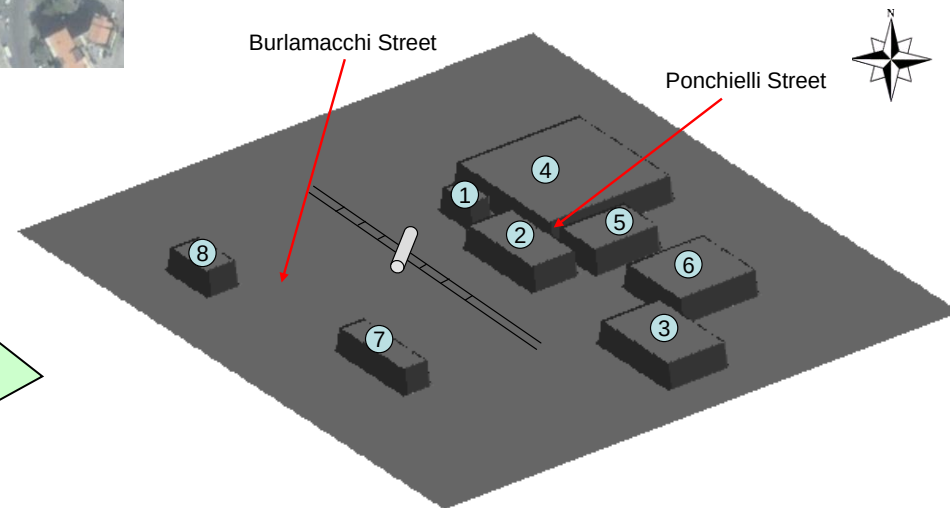
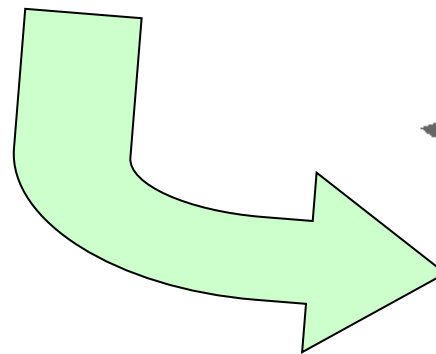




Google Earth



3D reconstruction of
Terminetto neighborhood





Simulation with TWODEE-2, a simulation code based on the Shallow Water Equations, *i.e.* equations based on depth-averaged variables to describe the flow behavior

$$\left\{ \begin{array}{l} \frac{\partial h}{\partial t} + \frac{\partial hu}{\partial x} + \frac{\partial hv}{\partial y} = u_e \\ \frac{\partial h(\rho - \rho_a)}{\partial t} + \frac{\partial h(\rho - \rho_a)u}{\partial x} + \frac{\partial h(\rho - \rho_a)v}{\partial y} = 0 \\ \frac{\partial h\rho u}{\partial t} + \frac{\partial h\rho u^2}{\partial x} + \frac{\partial h\rho uv}{\partial y} + S_1 \frac{\partial [g(\rho - \rho_a)h^2]}{\partial x} + S_1 g(\rho - \rho_a)h \frac{\partial e}{\partial x} + \frac{1}{2} \rho C_D u |\mathbf{u}| + V_x + k\rho_a \left[\frac{\partial}{\partial t} + u_a \frac{\partial}{\partial x} + v_a \frac{\partial}{\partial y} \right] h(u - u_a) = u_e \rho_a u_a \\ \frac{\partial h\rho v}{\partial t} + \frac{\partial h\rho vu}{\partial x} + \frac{\partial h\rho v^2}{\partial y} + S_1 \frac{\partial [g(\rho - \rho_a)h^2]}{\partial y} + S_1 g(\rho - \rho_a)h \frac{\partial e}{\partial y} + \frac{1}{2} \rho C_D v |\mathbf{u}| + V_y + k\rho_a \left[\frac{\partial}{\partial t} + u_a \frac{\partial}{\partial x} + v_a \frac{\partial}{\partial y} \right] h(v - v_a) = u_e \rho_a v_a \end{array} \right.$$

$$u_e = \frac{au_{ref}}{1 + b \text{ Ri}}$$

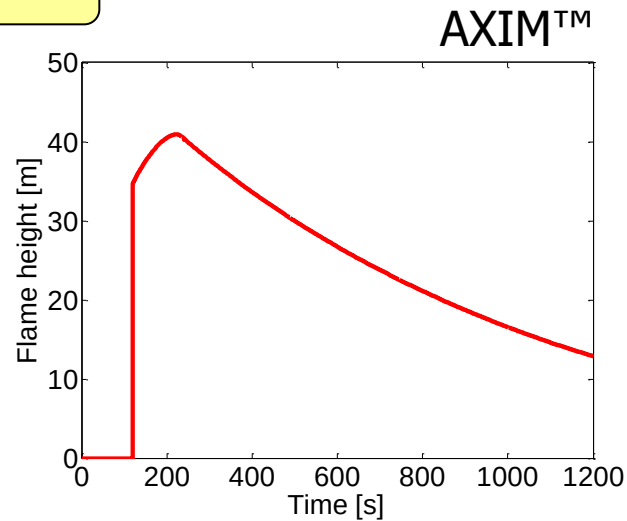
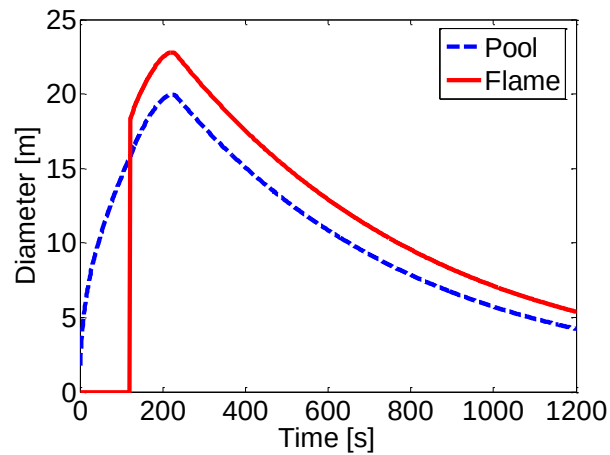
$$u_{ref}^2 = \mathbf{u}_*^2 + (\alpha_2 \mathbf{w}_*)^2 + \frac{1}{2} C_D \alpha_3^2 \mathbf{u}^2 + \alpha_7^2 |\mathbf{u} - \mathbf{u}_a|^2$$

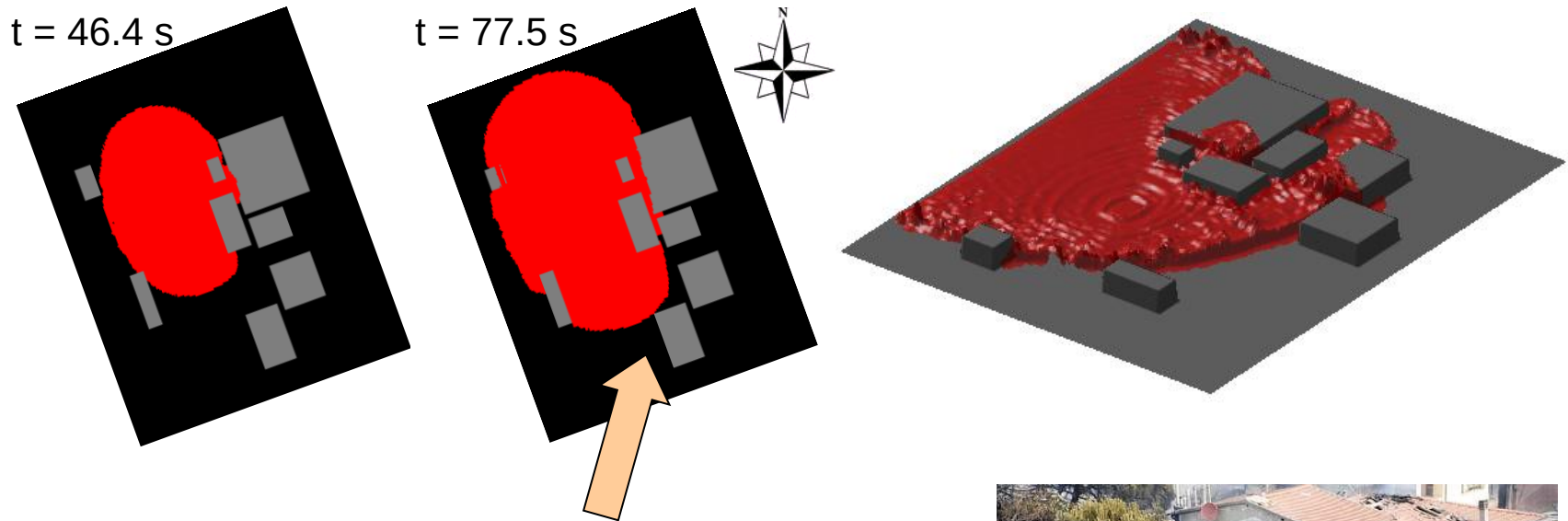


Risultati della simulazione



Ignition time: 2 min



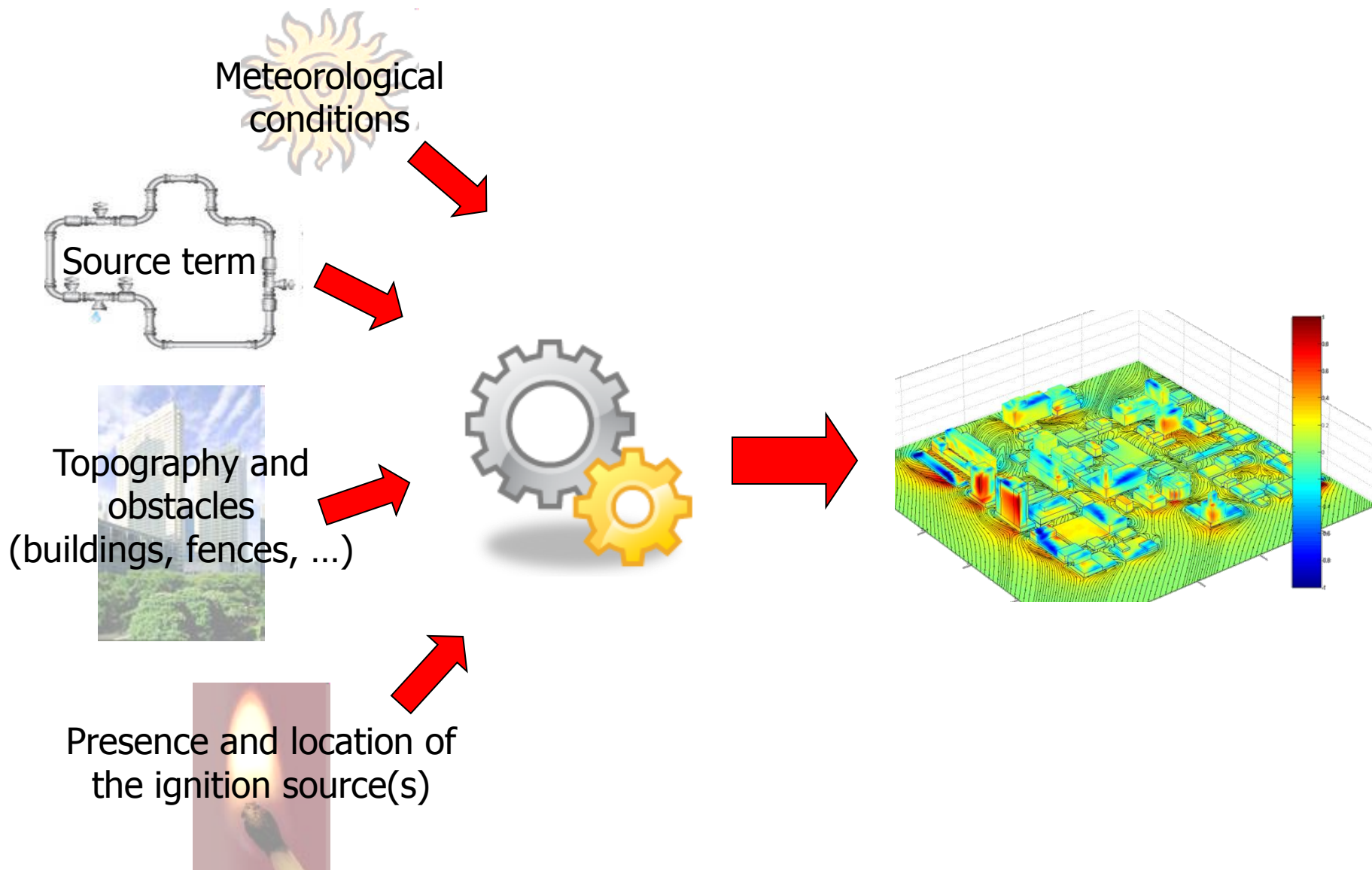


Arrival time of the gas-cloud to the farthest house that exploded ~ 80 s





Analisi e modellazione delle incertezze

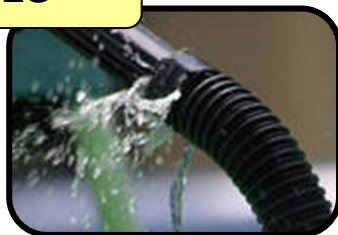




Storage conditions



Crack size



Ignition time



LPG composition



Meteorological conditions



Pool shape and area





Pool-fire size
(flame height)

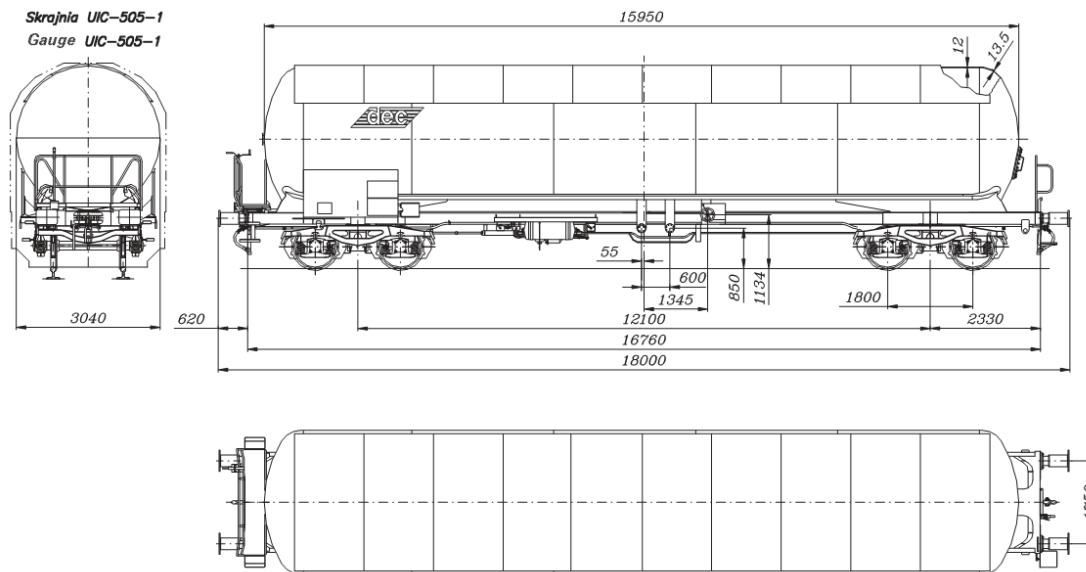




Initial tank car conditions	9 bar, 23°C
LPG mass	45 t
LPG composition	Pure propane
Crack size	100 cm ² , jagged-in sheet
Meteorological conditions	23°C, 0.5 m/s, NEE
Ignition time	2 min
Pool shape	Circular



Storage conditions



Storage conditions

Pressure [bar]	Boiling point	
9	296.15 K	23.00 °C
15	317.10 K	43.95 °C
20	330.51 K	57.36 °C
25	341.69 K	68.54 °C

← Ambient conditions

← Working pressure

23 °C, 9 bar

Total transported LPG : 630 t

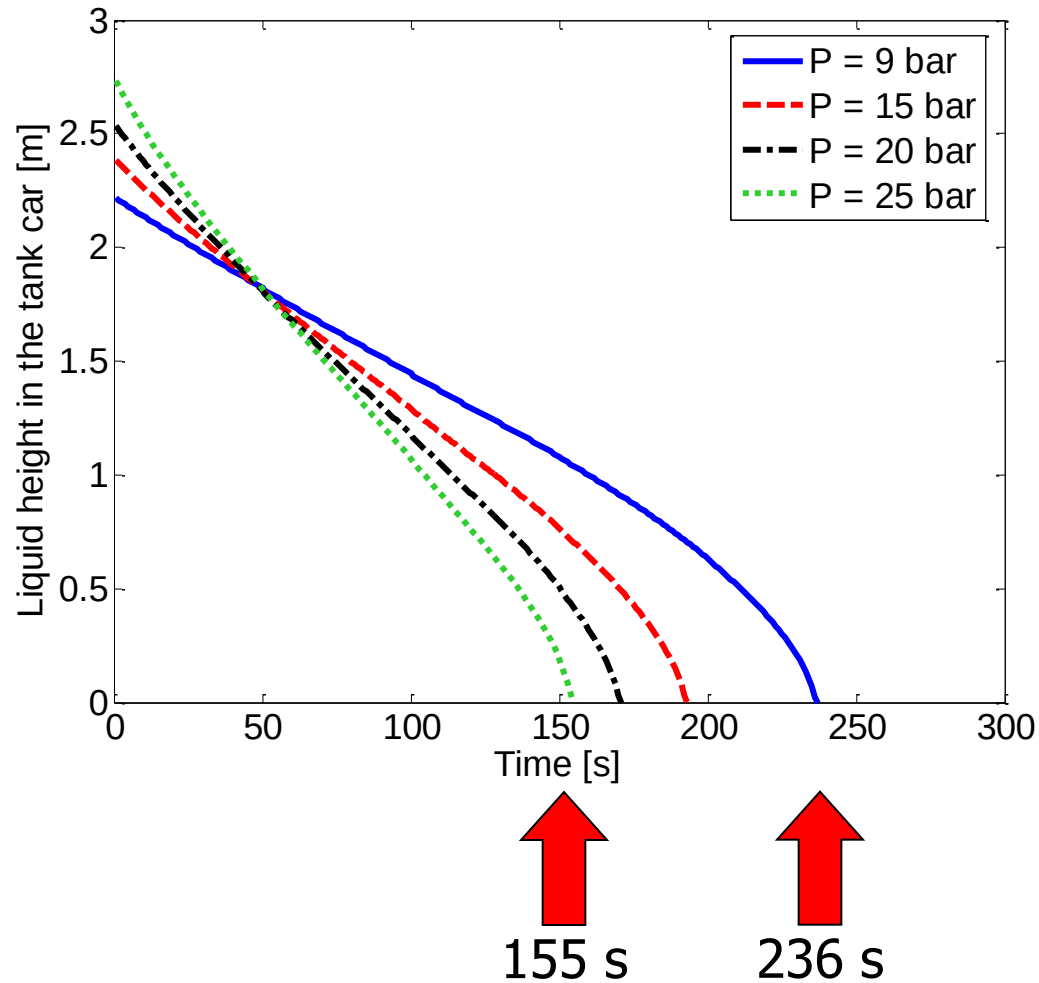
tank cars : 14

45 t/each

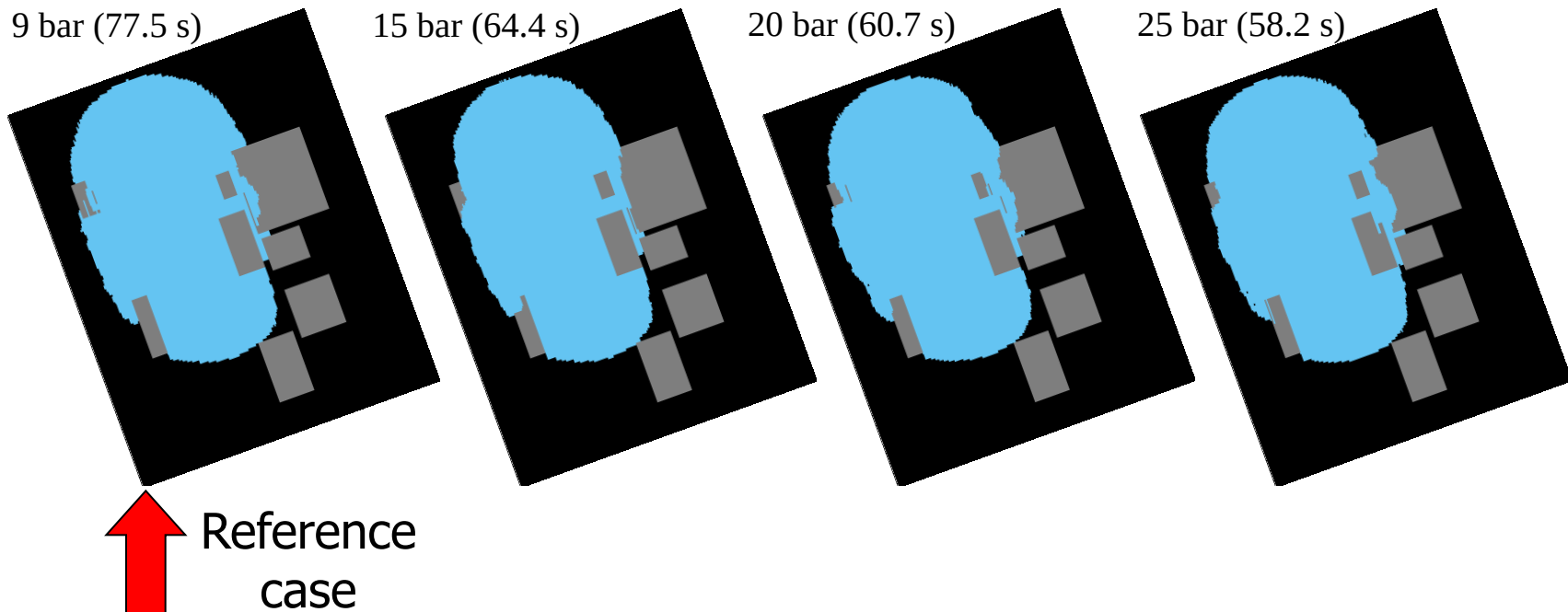


LPG release: storage conditions

47



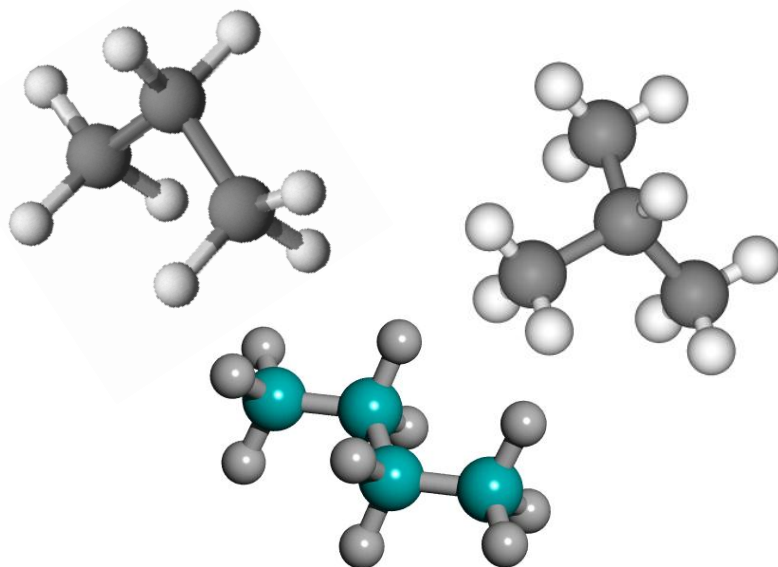
Initial pressure [bar]	Pool fire diameter [m]	Pool fire height [m]
9	22.8	40.9
15	14.2	28.7
20	Not occurred	Not occurred
25	Not occurred	Not occurred



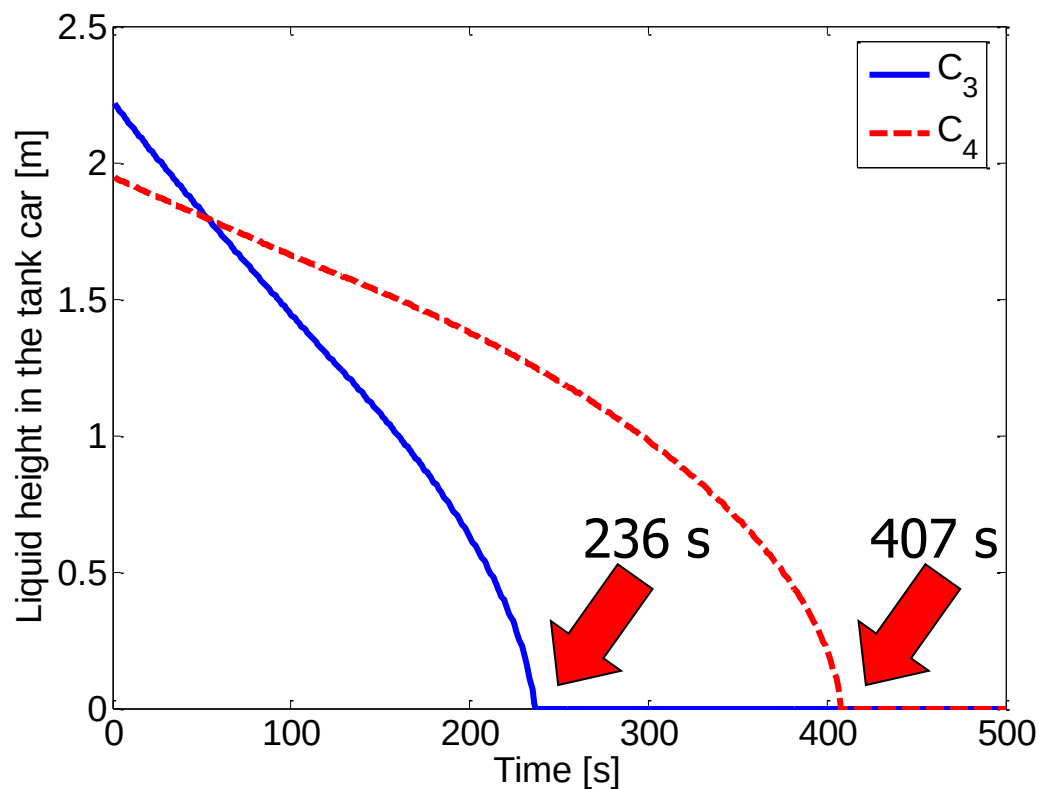
LPG composition

LPG is a variable mixture of C_3 and C_4 isomers

Its composition varies seasonally subject to specifications



Pure n-propane

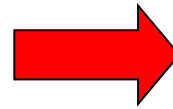


Composition	Pool fire diameter [m]	Pool fire height [m]
n-propane	22.8	40.9
n-butane	28.2	44.2



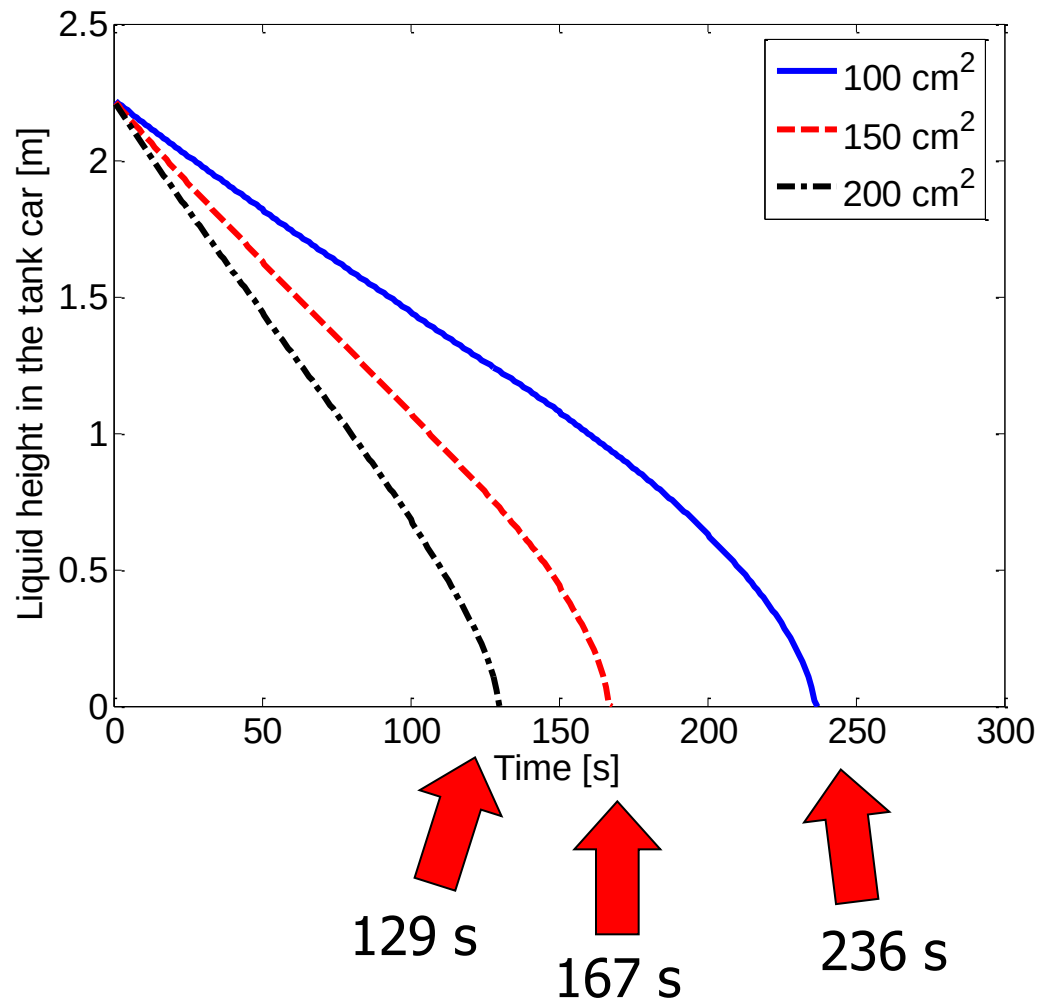
Crack size

Only a portion of the longitudinal mark was cut open



100 cm² trapezoidal hole
 $c_D = 0.62$ (jagged-in sheet)

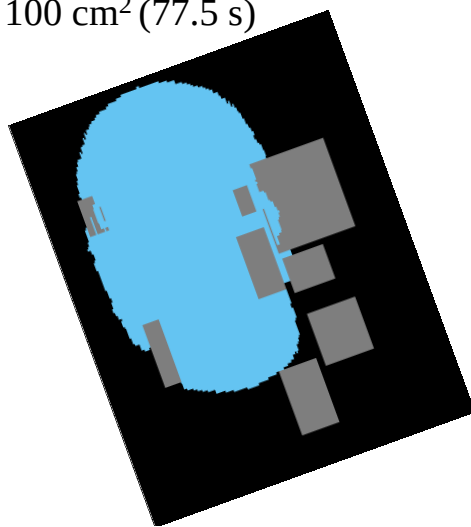




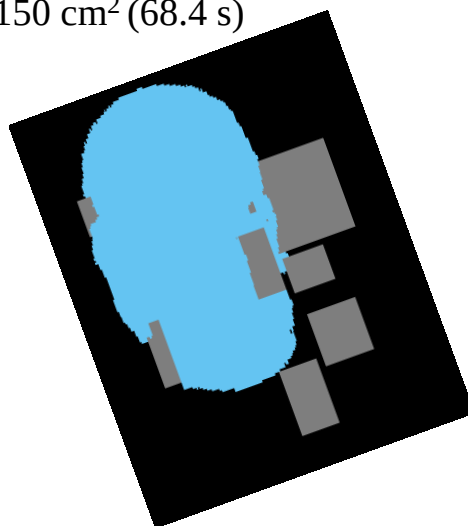


Crack area [cm ²]	Pool fire diameter [m]	Pool fire height [m]
100	22.8	40.9
150	25.5	44.5
200	26.5	45.8

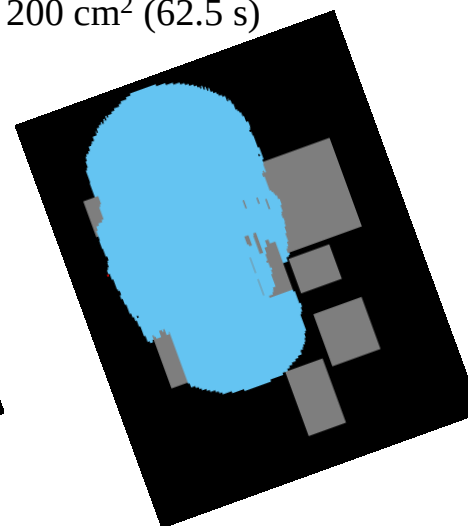
100 cm² (77.5 s)



150 cm² (68.4 s)



200 cm² (62.5 s)



Reference
case

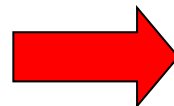


LPG release: meteorological conditions 54

Meteorological conditions

Report measured at the top of a hotel on the seafront of Viareggio about 1.7 km from the accident epicenter

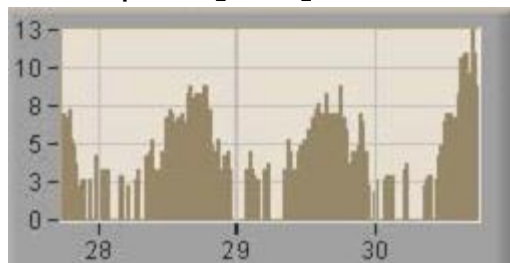
Wind direction	NEE
Wind speed [m/s]	< 1
Air temperature [°C]	23
Ambient pressure [mbar]	1008
Relative humidity	80%



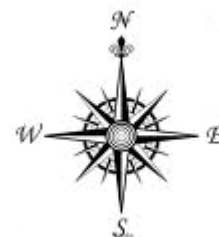
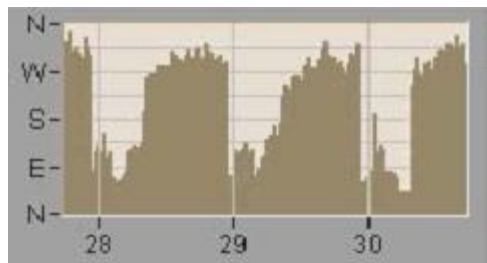
0.5 m/s
CALM CONDITIONS

NEE direction

Wind speed [knot]



Wind direction

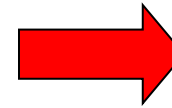




Ignition time

Some witnesses declared that the ignition occurred 2 min after the derailment, someone else reported 5 min.

The intense emotional involvement of the witnesses in those moments did not allow analyzing objectively the course of events.



2 min





Ignition time	1 min	2 min	5 min
Discharge time [s]	226	236	262
Gas cloud arrival time [s]	Not occurred	77.5	77.5
Pool fire diameter [m]	21.8	22.8	25.9
Pool fire height [m]	39.6	40.9	45.0



Pool shape and area

The liquid fraction spread on an irregular terrain and found some obstacles that limited a symmetric spreading.

The liquid was partially absorbed by the permeable ballast made of pebbles and rocks.



Circular pool
Unconfined pool





Conclusioni



There are a number of uncertainties that affect the accident reconstruction



Importance of parametric studies to determine:

- the worst-case scenario
- the most probable scenario
- the sensitivity of the accident consequences to input data

This analysis does not allow determining univocally the sequence and the timing of the events occurred in Viareggio



Nonetheless, it allows rejecting some scenarios, such as:

- **Initial tank car pressure of 20 and 25 bar**
- **Ignition at 1 min**



The gas cloud took ~ 80 s to reach the farthest exploded house (~ 100 m). This evidence confirms the need for effective mitigation measures because, in case of this type of accidents, there is no time to apply any emergency response actions.



CFD studies can identify the most effective mitigation measures, *e.g.*, barriers.



- **SIMULATION OF THE LPG RELEASE, DISPERSION, AND EXPLOSION IN THE VIAREGGIO RAILWAY ACCIDENT**
S. Brambilla, R. Totaro, D. Manca
Chemical Engineering Transactions, 19, 195-200, (2010)
- **A QUANTITATIVE ASSESSMENT OF THE VIAREGGIO RAILWAY ACCIDENT**
D. Manca, S. Brambilla, R. Totaro
Computer Aided Chemical Engineering, 28, 187-192, (2010)
- **THE VIAREGGIO LPG RAILWAY ACCIDENT: EVENT RECONSTRUCTION AND MODELING**
S. Brambilla, D. Manca
Journal of Hazardous Materials, 182, 346-357, (2010)
<http://dx.doi.org/10.1016/j.jhazmat.2010.06.039>
- **COMPLEXITY AND UNCERTAINTY IN THE ASSESSMENT OF THE VIAREGGIO LPG RAILWAY ACCIDENT**
D. Manca, S. Brambilla
Journal of Loss Prevention in the Process Industries, 23, 668-679, (2010)
<http://dx.doi.org/10.1016/j.jlp.2010.07.007>



- Collaboratori alla ricerca
 - Sara Brambilla (Post-doc, LANL, USA)
 - Roberto Totaro (Ph.D. student)





Grazie per l'attenzione